



1A Mill Hill, Shoreham-by-Sea, BN43 5TG

6th March 2026

ISSUE 02





CONTENTS

1	INTRODUCTION	3
2	NOISE CRITERIA	4
	2.1 NATIONAL PLANNING POLICY FRAMEWORK	4
	2.2 NOISE POLICY STATEMENT FOR ENGLAND	4
	2.3 PLANNING POLICY GUIDANCE	5
	2.4 BRITISH STANDARD 4142:2014	5
3	SITE SURVEYS.....	9
	3.1 SITE DESCRIPTION	9
	3.2 ENVIRONMENTAL SITE SURVEY PROCEDURE	10
4	NOISE SURVEY	11
5	NOISE IMPACT ASSESSMENT.....	11
	5.1 PROPOSED PLANT.....	11
	5.2 CLOSEST NOISE SENSITIVE RECEIVER.....	12
	5.3 NOISE EMISSION CRITERION	13
	5.4 BS4142 ASSESSMENT- Nearest Residential Window.....	13
	5.5 MITIGATION MEASURES.....	14
6	SUMMARY AND CONCLUSIONS.....	15
APPENDIX:		
A	ACOUSTIC TERMINOLOGY.....	16
B	CALCULATIONS	18
C	MEASUREMENTS	21
D	VIBRATION ISOLATION	22

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1.0 INTRODUCTION

Page | 3

DAA Group has been appointed to carry out a BS4142:2014+A1:2019 Noise Impact Assessment at 1A Mill Hill, Shoreham-by-Sea, BN43 5TG to support a Planning Application for the proposal of swimming pool plant in accordance with the provisions of:

- The National Planning Policy Framework
- The Noise Policy Statement for England (NPSE)
- The World Health Organisation Guidelines for Community Noise 1999 (WHO)
- Adur & Worthing Local Plan

The technical content of this assessment has been provided by a Tech member of the Institute of Acoustics.

The Institute of Acoustics is the UK's professional body for those working in acoustics, noise and vibration.

2.0 NOISE CRITERIA

2.1 NATIONAL PLANNING POLICY FRAMEWORK (NPPF)

The Department for Communities and Local Government introduced the National Planning Policy Framework (NPPF) in March 2012. The latest revision of the NPPF is dated December 2024.

The NPPF sets out the Government's planning policies for England and how these are expected to be applied. It provides a framework where local Councils can produce their own local and neighbourhood plans which reflect the needs of their communities.

In conserving and enhancing the natural environment, the planning system should prevent both new and existing development from contributing to, or being put at, unacceptable risk from environmental factors including noise.

Planning policies and decisions should aim to avoid noise giving rise to significant adverse impacts on health and quality of life as a result of new development. Conditions may be used to mitigate and reduce noise to a minimum so that adverse impacts on health and quality of life are minimised. It must be recognised that development will often create some noise and existing businesses wanting to develop in continuance of their business should not have unreasonable restrictions put on them. Reference is made within NPPF to the Noise Policy Statement for England (NPSE) as published by DEFRA in March 2010.

2.2 NOISE POLICY STATEMENT FOR ENGLAND (NPSE)

The long-term vision of the NPSE is stated within the documents scope, to 'promote good health and a good quality of life through the effective management of noise within the context of Government policy on sustainable development'. The policy aims are stated to:

- avoid significant adverse impacts on health and quality of life;
- mitigate and minimise adverse impacts on health and quality of life; and
- where possible, contribute to the improvement of health and quality of life.

The application of NPSE should mean that noise is properly taken into account at the appropriate time (for example in planning applications or appeals) where it must be considered alongside other relevant issues. The guiding principles of Government policy on sustainable development should be used to assist in the implementation of the NPSE.

The NPSE should apply to all types of noise apart from occupational noise in the workplace. The types of noises defined in the NPSE includes:

- Environmental noise from transportation sources;
- Neighbourhood noise which includes noise arising from within the community; industrial premises, trade and business premises, construction sites and noise in the street

The Noise Policy Statement England (NPSE) outlines observed effect levels relating to the above, as follows:

- **NOEL – No Observed Effect Level**

- o This is the level below which no effect can be detected. In simple terms, below this level, there is no detectable effect on health and quality of life due to the noise.

- **LOAEL – Lowest Observed Adverse Effect Level**

- o This is the level above which adverse effects on health and quality of life can be detected.

- **SOAEL – Significant Observed Adverse Effect Level**

- o This is the level above which significant adverse effects on health and quality of life occur.

As stated in The Noise Policy Statement England (NPSE), it is not currently possible to have a single objective based measure that defines SOAEL that is applicable to all sources of noise in all situations. Specific noise levels are not stated within the guidance for this reason, and allow flexibility in the policy until further guidance is available.

2.3 ProPG: PLANNING AND NOISE

As outlined above, the National Planning Policy Framework encourages improved standards of design, although it provides no specific noise levels which should be achieved on site for varying standards of acoustic acceptability, or a prescriptive method for the assessment of noise.

ProPG: Planning and Noise was published in May 2017 in order to encourage better acoustic design for new residential schemes in order to protect future residents from the harmful effects of noise. This guidance can be seen as the missing link between the current NPPF and

its predecessor, PPG24 (Planning Policy Guidance 24: Planning and Noise), which provided a prescriptive method for assessing sites for residential development, but without the nuance of 'good acoustic design' as outlined in ProPG.

ProPG allows the assessor to take a holistic approach to consider the site's suitability, taking into consideration numerous design factors which previously may not have been considered alongside the noise level measured on site, for example the orientation of the building in relation to the main source of noise incident upon it.

It should be noted this document is not an official government code of practice, and neither replaces nor provides an authoritative interpretation of the law or government policy, and therefore should be seen as a good practice document only.

2.4 BRITISH STANDARD 4142: 2014

British Standard (BS) 4142:2014 "Methods for rating and assessing industrial and commercial sound" describes methods for assessing the likely effects of sound on premises used for residential purposes.

It includes the assessment of sound from industrial and manufacturing processes, M&E plant and equipment, loading and unloading of goods and materials, and mobile plant/vehicles on the site. It can be used to assess sound from proposed, new, modified or additional industrial/commercial sources, at existing or new premises used for residential purposes.

The method described in BS4142: 2014 use outdoor sound levels to assess the likely effects of sound on people who might be inside or outside a dwelling or premises used for residential purposes upon which sound is incident.

The standard describes methods to measure and determine ambient, background and residual sound levels, and the rating levels of industrial/commercial sound. BS 4142: 2014 requires consideration of the level of uncertainty in the data and associated calculations.

BS 4142 is not intended to be used for the derivation or assessment of internal sound levels, or for the assessment of non-industrial / commercial sources such as recreational activities, motorsport, music and entertainment, shooting grounds, construction and demolition, domestic animals, people, and public address systems for speech.

The Reference Time Interval, T, is defined in the standard as the "specified interval over which the specific sound level is determined", which is 1 hour during the daytime (07:00 to 23:00 hours) and 15 minutes during the night (23:00 to 07:00 hours).

Ambient sound is defined in BS 4142: 2014 as "totally encompassing sound in a given situation at a given time, usually composed of sound from many sources near and far". It comprises the residual sound and the specific sound when present.

Residual sound is defined in BS 4142: 2014 as "ambient sound remaining at the assessment location when the specific sound source is suppressed to such a degree that it does not contribute to the ambient sound".

The background sound level is the LA90, T of the residual sound level, and is the underlying level of sound. Measurements of background sound level should be undertaken at the assessment location where possible or at a comparable location.

The measurement time interval should be sufficient to obtain a representative value (normally not less than 15 minutes) and the monitoring duration should reflect the range of background sound levels across the assessment period. The background sound level used for the assessment should be representative of the period being assessed.

The specific sound level is the LAeq,T of the sound source being assessed over the reference time interval, Tr. BS 4142: 2014 advises that Tr should be 1 hour during the day and 15 minutes at night.

The rating level is the specific sound level plus any adjustment for the characteristics of the sound (tone, impulse, intermittent or other acoustic feature). The standard describes subjective and objective methods to establish the appropriate adjustment. The adjustments for the different features and assessment methods are summarised in the table below.

Acoustic Feature Corrections in BS4142: 2014

Acoustic Feature	Adjustment for Acoustic Feature		
	Subjective Methods	Objective Methods	
Tonality	+2 dB if just perceptible +4 dB if clearly perceptible +6 dB if highly perceptible	Third Octave Analysis	Narrow Band Analysis
		+6 dB if tones identified	Sliding scale of 0 to +6 dB depending on audibility of tone
Impulsivity	+3 dB if just perceptible +6 dB if clearly perceptible +9 dB if highly perceptible	Sliding scale of 0 to +9 dB depending on prominence of impulsive sound	
Intermittency	+ 3 dB if intermittency is readily distinctive	n/a	
Other	+ 3 dB if neither tonal nor impulsive, but otherwise readily distinctive	n/a	

Where tonal and impulsive characters are present in the specific sound within the same reference period then these two corrections can both be taken into account. If one feature is dominant, it might be appropriate to apply a single correction. The rating level is equal to the specific sound level if there are no features present.

The level of impact is assessed by comparing the rating level of the specific sound source with the background sound level. Typically the greater the difference the greater the magnitude of the impact, depending on the context.

Other factors that may require consideration include the absolute level of sound, the character and level of the residual sound compared to the specific sound, and the sensitivity of the receptor and scope for mitigation.

When the rating level is above the background sound level, a difference of around +5 dB is likely to indicate an adverse impact and a difference of around +10 dB or more is likely to indicate a significant adverse impact, depending on the context.

The lower the rating level with respect to the background sound level, the less likely it is that the specific sound source will have an adverse impact. Where the rating level does not exceed the background sound level, this is an indication of the specific sound source having a low impact, depending on the context.

3.0 SITE SURVEYS

3.1 SITE DESCRIPTION

The site is located within a predominately residential area with the dominant source being road traffic noise from the surrounding roads. (See Figure 3.1)

Page | 7

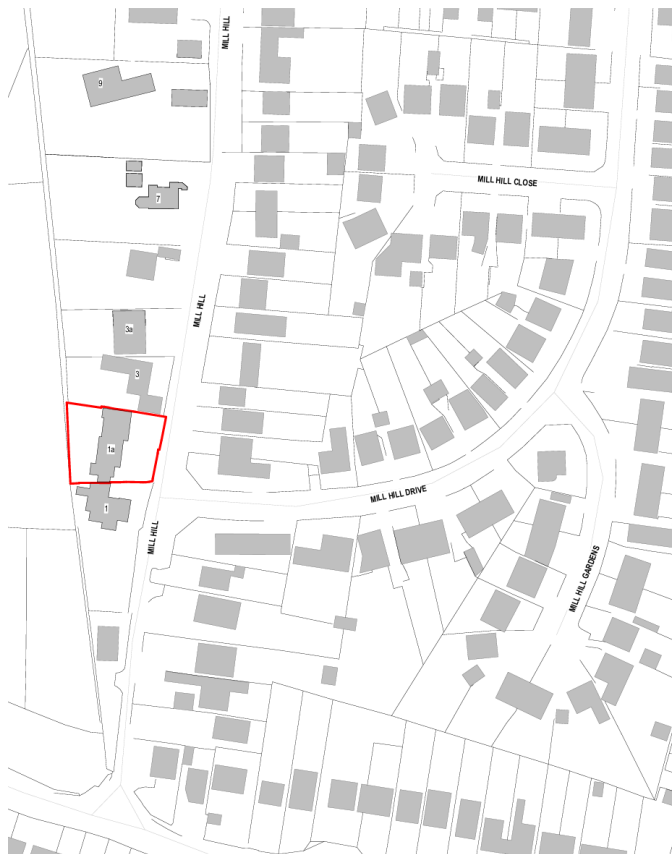


Figure 3.1 – Site Location

3.2 ENVIRONMENTAL SITE SURVEY PROCEDURE

In order to characterise the sound profile of the area at the closest sensitive receptor (NSR), an environmental sound survey has been carried out from 03/03/2026 to 04/03/2026. The monitoring position was chosen in order to collect representative sound levels at the NSR and the proposed location of the plant.

Noise Measurements were carried out free field at the rear façade of the application site in accordance with the principles of BS 7445: 2003: Description and Measurement of Environmental Noise. The monitoring location is shown in Figure 5.2.

3.3 EQUIPMENT

Instrument manufacturer	Cirrus Research Plc
Model	IEC 61672-3:2013
Serial Number	G302987
Microphone Type	MK:224
Serial Number	214457A
Cirrus CK: 675 Outdoor Kit	

All equipment used during the survey was field calibrated at the start and end of the measurement period with a negligible deviation of ≤ 0.5 dB. All sound level meters are calibrated every 24 months and all calibrators are calibrated every 12 months, by a third-party calibration laboratory. All microphones were fitted with a protective windshield for the entire measurements period.

3.4 METEOROLOGICAL CONDITIONS

All on site weather measurements have been compared with met office weather data of the area, specifically the closest weather station. When reviewing the time history of the noise measurements, any scenarios that were considered potentially to be affected by the local weather conditions have been omitted. The analysis of the noise data includes statistical and percentile analysis and review of minimum and maximum values, which aids in the preclusion of any periods of undesirable weather conditions. The weather conditions were deemed suitable for the measurement of environmental noise in accordance with BS7445 Description and Measurement of Environmental Noise. The table below presents the average temperature, wind speed and rainfall range for the 24-hour period during the entire measurement.

Weather Conditions				
Time Period	Air Temp (°C)	Rainfall mm/h	Prevailing Wind Direction	Wind Speed (m/h)
03/03/2026 – 11:00 – 23:59	6 – 15	0.0	ENE	2 – 5
04/03/2026 – 00:00 – 10:59	6 – 17	0.0	ENE	1 – 5

Table 3.4 – Weather Summary

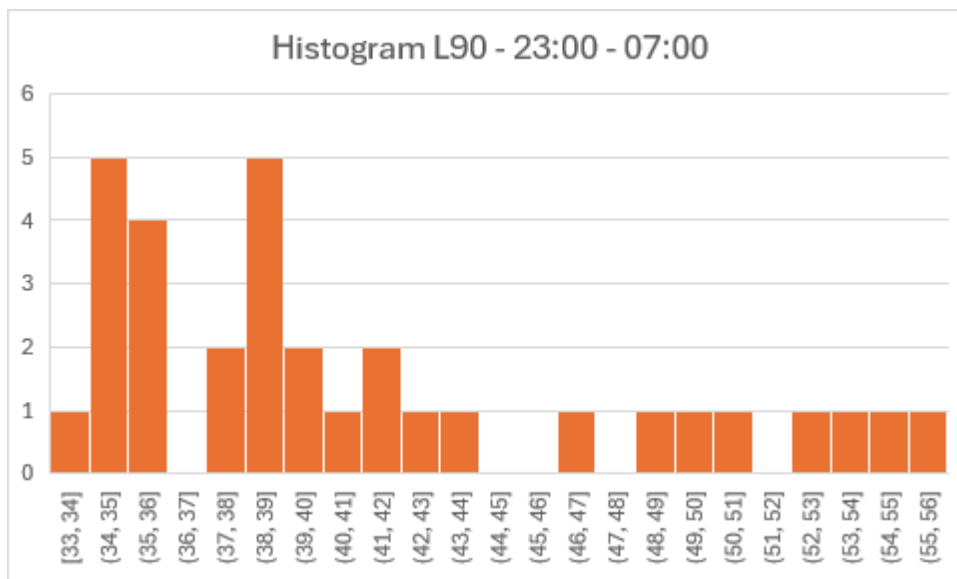
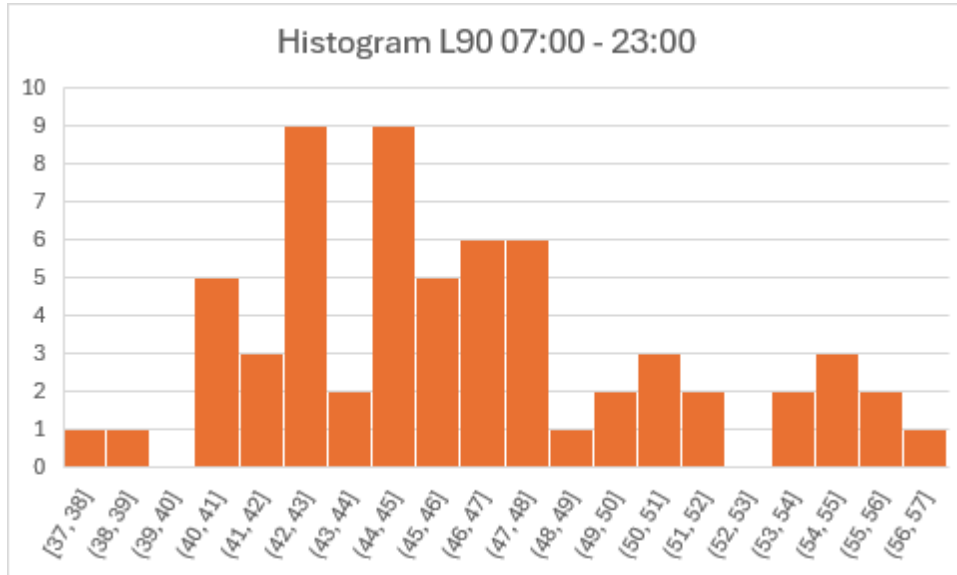
4.0 NOISE SURVEY

The background sound levels have been calculated in accordance with BS 4142:2014, which represents the most up-to-date guidance on the subject. Prior to the publication of the 2014 version of BS 4142, acousticians would use the lowest measured background sound levels; however, BS 4142: 2104 provides substantially more guidance on the determination of background sound levels. Section 8.1 of BS 4142: 2014 states that “for this purpose, the objective is not simply to ascertain a lowest measured background sound level, but rather to quantify what is typical during particular time periods. Among other considerations, diurnal patterns can have a major influence on background sound levels and, for example, the middle of the night can be distinctly different (and potentially of lesser importance) compared to the start or end of the night-time period for sleep purposes”. The guidance goes on to say that “a representative level ought to account for the range of background sound levels and ought not automatically to be assumed to be either the minimum or modal value”.

Period	LA90, 15
07:00 – 23.00	42dB
23:00 – 07:00	34dB

Table 4.1 Background Sound Level Summary Results

No existing plant was operating for the duration of the noise measurements.



5.0 NOISE IMPACT ASSESSMENT

5.1 PROPOSED PLANT

It is understood that the proposed plant is comprised of the following units:

- 1 x Integral dehumidification heat pump - Heatstar Andromeda EC 1000
- 1 x Invermaster pump

Proposed Plant	Swl (dB(A))
Heatstar Andromeda EC 1000 - Outlet	76
Heatstar Andromeda EC 1000 - Inlet	73
	Spl (dB(A))
Invermaster pump	55

Table 5.1 – Manufacturer supplied Sound levels

Sound Data:

Linear Sound Power	Frequency Hz	Return air	Supply air
<i>L_w dB :</i>	63	67.9	65.1
	125	69.1	66.2
	250	66.9	64.1
	500	67.9	65.1
	1000	65.1	62.3
	2000	66.9	64.1
	4000	64.3	61.5
	8000	55.4	52.6

Table 5.1.1 – Manufacturer data

N.b All plant will be located within the plant room

5.2 CLOSEST NOISE SENSITIVE RECEIVER

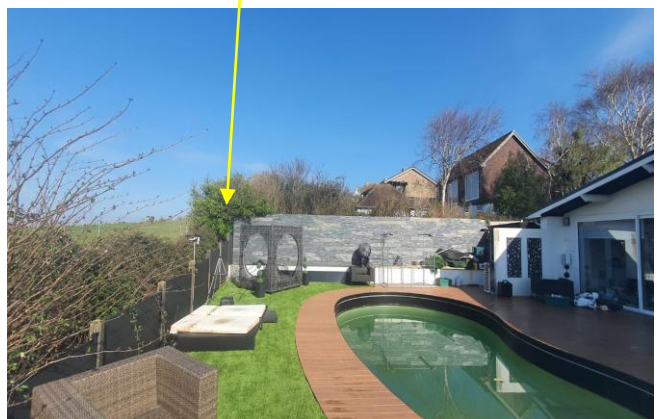
The closest noise sensitive receiver to the proposed plant room has been identified as being a residential window located approximately 20 meters away as shown in Figure 5.2.

Page | 12



Figure 5.2 –Plant Location

	Proposed Location of Plant room
	Nearest Residential Noise Sensitive Window
	Measurement Location



5.3 NOISE EMISSION CRITERION

It is understood that the proposed operating hours is intermittent over 24hrs.

It is determined that the proposed plant is not considered to contain tones. We have added a 3dB correction for intermittency.

Page | 13

The criteria for plant sound, to be achieved at a point 1m from the closest noise sensitive window, has been set as shown in Table 5.3 in order to comply with the Local Authority requirements.

Time Period	Noise Criterion at Nearest Residential Receiver
07:00 – 23:00	32
23:00 – 07:00	24

Table 5.3 - Proposed noise emissions criterion

5.4 BS4142 ASSESSMENT – Nearest Residential Window

BS4142:2014 Assessment	
Source	Pool Plant
Operating Period	24hrs
Reference Time Interval (Tr)	15 minutes
Element	Level (dB)
Specific Sound Level	17
Representative Background Noise Level (LA90)	34
Corrections	6
Rating Level	23
Excess of Rating over Background Sound Level	-11

Detailed calculations are shown in Appendix B.

5.5 MITIGATION MEASURES

5.5.1 – Noise Emissions

In order to achieve the specific sound level and subsequent rating level shown in the assessment above, the following mitigation measures are required.

To reduce duct breakout on the outlet of the Heatstar Andromeda EC 1000 an attenuator is required to be fitted on the discharge side of the fan similar to an Acoustica R02-2-600 with the below insertion losses:

<i>Outlet</i>	<i>INSERTION LOSS (dB) – CENTRE BAND FREQUENCY</i>							
Hz	63	125	250	500	1K	2K	4K	8K
R02-2-600	7	12	20	31	39	40	38	27

To reduce duct breakout on the inlet of the Heatstar Andromeda EC 1000 an attenuator is required to be fitted on the atmospheric side of the fan similar to an Acoustica CP01-M31-120 with the below insertion losses:

<i>Inlet</i>	<i>INSERTION LOSS (dB) – CENTRE BAND FREQUENCY</i>							
Hz	63	125	250	500	1K	2K	4K	8K
CP01-M31-120	6	9	14	23	32	32	18	15

In addition to the control of airborne noise transfer, it is important to consider the transfer of noise as vibration to adjacent properties as well as any sensitive areas of the same building. The plant should be isolated from the structure of the building using anti-vibration. The isolators shall incorporate rubber or neoprene high-frequency isolation pads. Antivibration mounts are widely available from suppliers/installers often in pedestal rubber mountings. See Appendix D for more details.



6.0 SUMMARY AND CONCLUSIONS

DAA Group has been appointed to carry out a Noise Impact Assessment at 1A Mill Hill, Shoreham-by-Sea, BN43 5TG. The purpose of the survey was to assess the level of noise emanating from the proposed pool plant to the nearest noise sensitive residential window and to advise on the level and type of mitigation that will be required.

Page | 15

Manufacturer's noise data of proposed plant has been used to obtain Specific and Rated Noise Level at the nearest noise sensitive receiver in accordance with British Standard BS4142:2014 for compliance with Adur & Worthing Council requirements.

The rating level was compared with the representative background noise level to assess the likelihood of impact considering the environmental noise context of the area as per the requirements of BS4142:2014.

It has been concluded that noise emissions from the proposed plant would not have an adverse impact on the nearest residential receivers provided the mitigation measures in 5.5 are carried out.

APPENDIX A ACOUSTIC TERMINOLOGY

B.1 WEIGHTED DECIBEL, dB(A)

The unit generally used for measuring environmental, traffic or industrial noise is the A-weighted sound pressure level in decibels, denoted dB(A). The weighting is based on the frequency response of the human ear and has been found to correlate well with human subjective reactions to various sounds. An increase or decrease of approximately 10 dB corresponds to a subjective doubling or halving of the loudness of a noise, and a change of 2 to 3 dB is subjectively barely perceptible.

Page | 16

B.2 EQUIVALENT CONTINUOUS SOUND LEVEL, L_{Aeq}

Another index for assessment for overall noise exposure is the equivalent continuous sound level, L_{Aeq} . This is a notional steady level which would, over a given period, deliver the same sound energy as the actual time-varying sound over the same period.

B.3 MAXIMUM NOISE LEVEL, L_{Amax}

The maximum noise level identified during a measurement period. Experimental data has shown that the human ear does not generally register the full loudness of transient sound events of less than 125 ms in duration.

B.4 NOISE RATING, NR

Noise ratings are used as a single figure criterion for specifying services noise in buildings. Each noise rating value has an associated spectrum of defined values in each third or octave frequency band. To determine the noise rating of a room the measured spectrum is compared to a set of noise rating curves. The highest NR curve that crosses any single frequency band of the measurement determines the noise rating for the room.

The single figure noise rating is read at the 1 kHz band.

B.5 SOUND LEVEL DIFFERENCE (D)

The sound insulation required between two spaces may be determined by the sound level difference needed between them. A single figure descriptor which characterises a range of frequencies, the weighted sound level difference, D, is sometimes used (BS EN ISO 717-1). This parameter is not adjusted to reference conditions.

The standardized level difference, D_n , T is a measure of the difference in sound level between two rooms, in each frequency band, where the reverberation time in the receiving room has been normalised to 0.5 s. This parameter measures all transmission paths, including flanking paths.

The weighted standardized level difference, D_{nTw} , is a measure of the difference in sound level between two rooms, which characterises a range of frequencies and is normalised to a reference reverberation time

B.6 SOUND REDUCTION INDEX (R)

The sound reduction index (or transmission loss) of a building element is a measure of the loss of sound through the material, i.e. its attenuation properties. It is a property of the component, unlike the sound level difference which is affected by the common area between the rooms and the acoustic of the receiving room. The weighted sound reduction index, R_w , is a single figure description of sound reduction index characterising a range of frequencies, which is defined in BS EN ISO 717-1: 1997. The R_w is calculated from measurements in an acoustic laboratory

B.7 STATISTICAL NOISE LEVELS ($L_{A90, (T)}$ $L_{A1, (T)}$ $L_{A10, (T)}$ etc.)

For levels of noise that vary widely with time, for example road traffic noise, it is necessary to employ an index which allows for this variation. The L_{A10} is the level exceeded for ten per cent of the time under consideration, has historically been

adopted in the UK for the assessment of road traffic noise. The L_{A90} is the level exceeded for ninety per cent of the time, has been adopted to represent the background noise level. The L_{A1} the level exceeded for one per cent of the time, is representative of the maximum levels recorded during the sample period. A weighted statistical noise levels are denoted $L_{A10, dB}$ $L_{A90, dB}$ etc. The reference time (T) is normally included, e.g. $L_{A10, (5min)}$, & $L_{A90, (8hr)}$.

B.8 TYPICAL NOISE LEVELS

Typical noise levels are given in the following table.

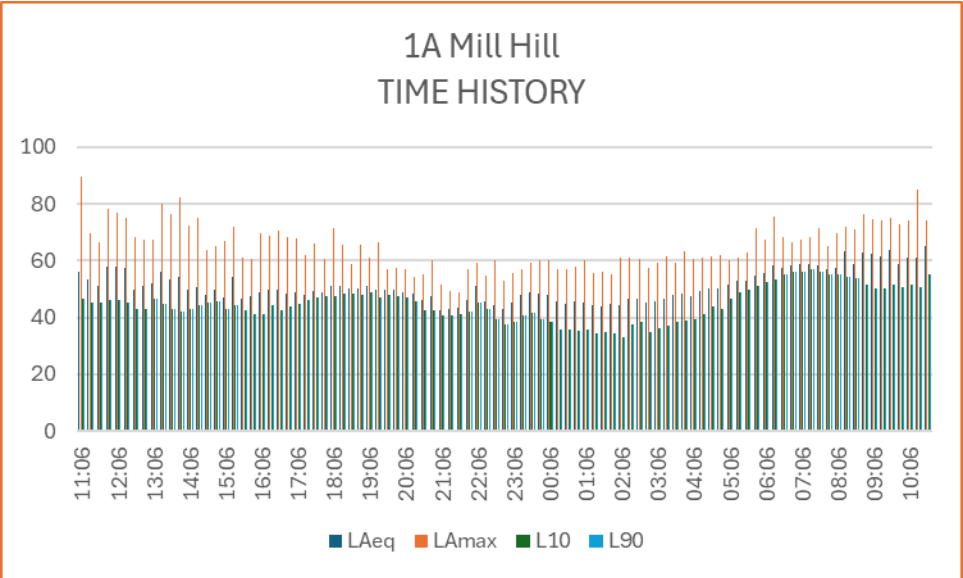
Noise Level dB(A)	Example
130	Threshold of pain
120	Jet aircraft take-offs at 100 m
110	Chain saw at 1 m
100	Inside disco
90	Heavy lorries at 5 m
80	Kerbside of busy street
70	Loud radio (in typical domestic room)
60	Office or restaurant
50	Domestic fan heaters at 1m
40	Living room
30	Ventilation Noise in Theatre
20	Remote countryside on still night
10	Sound insulated test chamber
0	Threshold of hearing.

APPENDIX B CALCULATIONS

Outlet Fan														
NOISE EMISSION CALCULATION														
ITEM	PARAMETER				HZ	63	125	250	500	1K	2K	4K	8K	dB
1	Schedule of Plant		Qty											
2														
3	Model: Heatstar Andromeda EC 1000	1	Swl	dB	+	68	69	67	68	65	67	64	55	76
4	Ductwork Natural Losses		Lo	IL	dB	-	15	10	3	2	6	8	8	9
5	Attenuator Model:R02-2-600	1	IL	dB	-	7	12	20	31	39	40	38	27	
6														
7														
8														
9														
10														
11	Revised Sound Power Level:	1	Swl	dB	+	46	47	44	35	20	19	18	19	51
12														
13														
14														
15	Distance to nearest receptor Metres:	r	20	dB	-	37	37	37	37	37	37	37	37	37
16	SPL=SWL -20log(r) + 10log(Q) -11 dB.	Q	1											
17														
18														
19														
20	Spl at receptor			dB	+	9	10	7	-2	-17	-18	-19	-18	14
21														
22														
23	Façade correction	3	dB	+	3	3	3	3	3	3	3	3	3	3
24	Intermittancy Correction	3	dB	+	3	3	3	3	3	3	3	3	3	3
25														
26														
27	Specific noise level at receptor			dB	+	15	16	13	4	-11	-12	-13	-12	20
28	(1m outside noise sensitive window)													
29	Background Noise Levels: (L _{A90})													
30	07:00 - 23:00			dB	+									42
31	Difference: (Daytime Assessment level)			dB	-									-22
32														
33	E&OE													
34	Night time (23:00-07:00)			dB	+									34
35	Difference: (Daytime Assessment level)			dB	-									-14
36														
	E&OE													

Inlet Fan														
NOISE EMISSION CALCULATION														
ITEM	PARAMETER			HZ		63	125	250	500	1K	2K	4K	8K	dB
1	Schedule of Plant		Qty											
2														
3	Model: Heatstar Andromeda EC 1000	1	Swl	dB	+	65	66	64	65	62	64	62	53	73
4	Ductwork Natural Losses	Lo	IL	dB	-	15	10	3	2	6	8	8	9	
5	Attenuator Model:CP01-M31-120	1	IL	dB	-	6	9	14	23	32	32	18	15	
6														
7														
8														
9														
10														
11	Revised Sound Power Level:	1	Swl	dB	+	44	47	47	40	24	24	36	29	51
12														
13														
14														
15	Distance to nearest receptor Metres:	r	20	dB	-	37	37	37	37	37	37	37	37	37
16	$SPL = SWL - 20\log(r) + 10\log(Q) - 11$ dB.	Q	1											
17														
18														
19														
20	Spl at receptor			dB	+	7	10	10	3	-13	-13	-1	-8	14
21														
22														
23	Façade correction	3		dB	+	3	3	3	3	3	3	3	3	3
24	Intermittancy Correction	3		dB	+	3	3	3	3	3	3	3	3	3
25														
26														
27	Specific noise level at receptor			dB	+	13	16	16	9	-7	-7	5	-2	20
28	(1m outside noise sensitive window)													
29	Background Noise Levels: (L_{A90})													
30	07:00 - 23:00			dB	+									42
31	Difference: (Daytime Assessment level)			dB	-									-22
32														
33	E&OE													
34	Night time (23:00-07:00)			dB	+									34
35	Difference: (Daytime Assessment level)			dB	-									-14
36														
	E&OE													

PARAMETER			HZ	63	125	250	500	1K	2K	4K	8K	dBA
Schedule of Plant	Qty											
Invermaster Pool Pump	1	Spl	dB +									55
SRI of Plant Room		IL	dB -									34
Revised Spl:	1	Spl	dB +									21
Distance to nearest receptor Metres:	20		dB -									-26
$SPL=L1-20\log_{10}(r2/r1)$	1											
Spl at receptor			dB +									-5
Façade correction	3.0		dB +									3
Intermittant noise correction	3		dB +									3
Specific noise level at receptor (1m outside noise sensitive window)			dB +									1
Background Noise Levels:(L_{A90})												
Daytime (07:00-23:00)												42
Difference: (Assessment level)			dB -									-41
Night Time (23:00-07:00)												34
Difference: (Assessment level)			dB -									-33
E&OE												



Vibration Isolation

CMS – Kinetics Model AC¹³

KINETICS™ Fiberglass Isolators Model AC



Description

Model AC Fiberglass Isolators consist of a molded inorganic fiberglass isolation pad bonded to a steel load transfer plate and to a formed steel bolt-down bracket and include an equipment anchor bolt with a neoprene grommet to prevent metal-to-metal contact. Fiberglass pads are fine (0.00027"/6.8 microns diameter) bonded annealed glass fibers which are stabilized by pre-compressing the material during manufacture and then coated with a flexible moisture-impervious elastomeric membrane. Fiberglass is unique in that the natural frequency is constant over a wide operating load range and the stiffness increases proportionately with load applied. Model AC Fiberglass Isolators are available in sizes with capacities from 40 to 900 lbs. (18 kg-409 kg) and deflections of 0.18" to 0.70" (4mm-18mm). Kinetics Model AC Isolators are recommended for the isolation of vibration produced by utility ventilating fans, vane axial fans, high speed motors, roof-mounted exhaust fans, and similar mechanical equipment.

Features

- Inorganic fiberglass media
- Flexible elastomeric coating
- Constant natural frequency over a wide load range
- Predictable dynamic response
- High energy dissipation
- Controlled viscous damping
- Load capacities 40 lbs. to 900 lbs. (18kg-409kg)
- Rated static deflection 0.18" to 0.70" (4mm-18mm)
- Steel load transfer plate
- Steel bolt and hold-down support bracket

Application

Kinetics Model AC Fiberglass Isolators can be used for any application requiring isolation of audible frequency vibration, or noise, or for vibration isolation of mechanical equipment with lowest operating speeds of 1750 RPM when mounted on a grade-supported slab or pier.

Model AC isolators are typically used when the predictable dynamic response and permanent load support characteristics of fiberglass are desired in conjunction with a bolt-down and vertical lift control feature.

Typical uses of Model AC isolators include the support and isolation of utility ventilating fans, vane axial fans, motors, roof-mounted exhaust fans, and similar mechanical equipment.

Special application of Model AC isolators have included use as both an isolator and wind lift hold-down support for isolated precast concrete roof systems used to reduce transmitted noise from fly-over aircraft.

Use Model AC mounts when Kinetics fiberglass isolators are recommended and it is desirable to bolt equipment to supporting structures.

¹³ Supplied by CMS Acoustics (UK).

CMS – Kinetics Model AC

Specifications

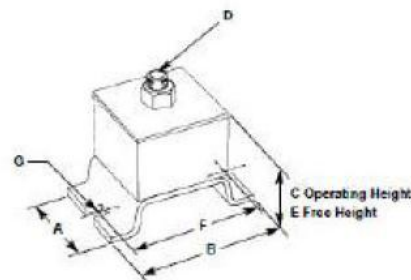
Vibration isolators shall be precompressed molded fiberglass pads individually coated with flexible, moisture-impervious elastomeric membranes. Vibration isolation pads shall be molded from glass fibers with fiber diameters not exceeding 0.00027" (6.8 microns) and with a modulus of elasticity of 10.5 million PSI (750.00 kg per sq. cm).

Natural frequency of fiberglass vibration isolators shall be essentially constant for the operating load range of the supported equipment.

Vibration isolators shall be bonded to a steel load transfer plate and a formed steel bolt-down bracket and shall also include an equipment mounting bolt with a neoprene grommet to prevent metal-to-metal contact.

Vibration isolators shall be selected by the manufacturer for each specific application to comply with deflection requirements as shown on the Vibration Isolation Schedule or as indicated on the project documents.

Vibration isolators shall be model AC, as manufactured by Kinetics Noise Control, Inc.



Isolator Type	Capacity Range	Maximum Deflection	Dimensions						
			A	B	C*	D	E	F	G
AC-221L	40-200 lbs.	0.27"	2.60"	4.75"	1.98"	0.39"	3.25"	3.75"	0.44"
AC-221G	100-400 lbs.	0.12"	2.50"	4.75"	2.07"	0.50"	3.25"	3.75"	0.44"
AC-331L	90-450 lbs.	0.35"	3.00"	4.75"	1.90"	0.38"	3.25"	3.75"	0.44"
AC-331G	225-900 lbs.	0.27"	3.00"	4.75"	1.98"	0.38"	3.25"	3.75"	0.44"
AC-222G	20-100 lbs.	0.65"	2.50"	4.75"	2.50"	0.50"	3.25"	3.75"	0.44"
AC-222L	40-200 lbs.	0.52"	2.50"	4.75"	2.71"	0.38"	3.25"	3.75"	0.44"
AC-222Q	100-400 lbs.	0.30"	2.50"	4.75"	2.65"	0.50"	3.25"	3.75"	0.44"
AC-332-L	90-450 lbs.	0.70"	3.00"	4.75"	2.50"	0.50"	3.25"	3.75"	0.44"
AC-332Q	225-400 lbs.	0.52"	3.00"	4.75"	2.71"	0.38"	3.25"	3.75"	0.44"
AC-221L	15-61 kg	6 mm	65 mm	121 mm	50 mm	9.8 mm	87 mm	95 mm	11 mm
AC-221G	45-182 kg	4 mm	63 mm	121 mm	52 mm	9.6 mm	87 mm	95 mm	11 mm
AC-331L	41-205 kg	9 mm	76 mm	121 mm	48 mm	9.6 mm	87 mm	95 mm	11 mm
AC-331G	102-405 kg	6 mm	76 mm	121 mm	50 mm	9.6 mm	87 mm	95 mm	11 mm
AC-222G	9-44 kg	17 mm	63 mm	121 mm	66 mm	9.6 mm	83 mm	95 mm	11 mm
AC-222L	15-91 kg	14 mm	63 mm	121 mm	69 mm	9.6 mm	83 mm	95 mm	11 mm
AC-222Q	45-182 kg	9 mm	63 mm	121 mm	73 mm	9.6 mm	83 mm	95 mm	11 mm
AC-332-L	41-205 kg	18 mm	76 mm	121 mm	66 mm	9.6 mm	83 mm	95 mm	11 mm
AC-332Q	102-405 kg	14 mm	76 mm	121 mm	69 mm	9.6 mm	83 mm	95 mm	11 mm

*Operating height varies with applied load.



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Kinetics Noise Control, Inc. is continually upgrading the quality of our products. We reserve the right to make changes to this and all products without notice.

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